Designer's™ Data Sheet

ISOTOP™ TMOS E-FET ™ Power Field Effect Transistor

N-Channel Enhancement-Mode Silicon Gate

This advanced high voltage TMOS E-FET is designed to withstand high energy in the avalanche mode and switch efficiently. This new high energy device also offers a drain-to-source diode with fast recovery time. Designed for high voltage, high speed switching applications such as power supplies, PWM motor controls and other inductive loads, the avalanche energy capability is specified to eliminate the guesswork in designs where inductive loads are switched and offer additional safety margin against unexpected voltage transients.

- 2500 V RMS Isolated Isotop Package
- Avalanche Energy Specified
- Source—to—Drain Diode Recovery Time Comparable to a Discrete Fast Recovery Diode
- Diode is Characterized for Use in Bridge Circuits
- Very Low Internal Parasitic Inductance
- IDSS





ELECTRICAL CHARACTERISTICS ($T_J = 25^{\circ}C$ unless otherwise noted)

Characteristic		Symbol	Min	Тур	Max	Unit
OFF CHARACTERISTICS				•		
Drain-Source Breakdown Voltage (V _{GS} = 0 Vdc, I _D = 250 μAdc) Temperature Coefficient (Positive)		V(BR)DSS	200 —	215 250		Vdc mV/°C
Zero Gate Voltage Drain Current (VDS = 200 Vdc, VGS = 0 Vdc) (VDS = 200 Vdc, VGS = 0 Vdc, TJ = 125°C)		I _{DSS}	[]	[]	10 100	μAdc
Gate–Body Leakage Current ($V_{GS} = \pm 20 \text{ Vdc}, V_{DS} = 0$)		IGSS	_	_	200	nAdc
ON CHARACTERISTICS (1)						
Gate Threshold Voltage $(V_{DS} = V_{GS}, I_D = 250 \mu\text{Adc})$ Threshold Temperature Coefficient (Negative)		^V GS(th)	2.0 —	3.0 —	4.0 —	Vdc mV/°C
Static Drain–Source On–Resistance (V _{GS} = 10 Vdc, I _D = 62.5 Adc)		R _{DS(on)}		12	15	mOhm
Drain–Source On–Voltage ($V_{GS} = Vdc$) ($I_D = 125 \text{ Adc}$) ($I_D = 62.5 \text{ Adc}$, $T_J = 125^{\circ}C$)		V _{DS(on)}	_	_	2.1 1.9	Vdc
Forward Transconductance (V _{DS} = 15 Vdc, I _D = 62.5 Adc)		9FS	50	80	_	mhos
DYNAMIC CHARACTERISTICS				•		
Input Capacitance	(V _{DS} = 25 Vdc, V _{GS} = 0 Vdc, f = 1.0 MHz)	C _{iss}	_	14400	_	pF
Output Capacitance		Coss	_	3600	_	
Reverse Transfer Capacitance		C _{rss}	_	920	_	
SWITCHING CHARACTERISTICS (2)			•		•
Turn-On Delay Time	$(V_{DD} = 250 \text{ Vdc}, I_{D} = 125 \text{ Adc}, V_{GS} = 10 \text{ Vdc}, R_{G} = 4.7 \Omega)$	^t d(on)	_	72	_	ns
Rise Time		t _r	_	574	_	
Turn-Off Delay Time		^t d(off)	_	327	_	
Fall Time		t _f	_	376	_	
Gate Charge	(V _{DS} = 160 Vdc, I _D = 125 Adc, V _{GS} =10 Vdc)	QT	_	510	_	nC
		Q ₁	_	100	_	
		Q ₂	_	245	_	
		Q ₃	_	158	_	1
SOURCE-DRAIN DIODE CHARAC	TERISTICS					
Forward On–Voltage (1)	(I _S = 125 Adc, V _{GS} = 0 Vdc) (I _S = 125 Adc, V _{GS} = 0 Vdc, T _J = 125°C)	V _{SD}	_ _	1.00 1.00	1.5 —	Vdc
Reverse Recovery Time	(I _S = 125 Adc, V _{GS} = 0 Vdc, dI _S /dt = 100 A/μs)	t _{rr}	_	310	_	ns
		ta	_	220	_	
		t _b	_	90	_	
Reverse Recovery Stored Charge		Q _{RR}	_	9.2	_	μС
NTERNAL PACKAGE INDUCTANO	ČE .	-	-	-	-	-
Internal Drain Inductance (Measured from contact screw on tab to center of die) (Measured from the drain lead 0.25" from package to center of die)		L _D	_ _	3.5 5.0	_	nH
Internal Source Inductance (Measured from the source lead 0.25" from package to source bond pad)		LS	_	5.0	_	nH

⁽¹⁾ Pulse Test: Pulse Width ≤ 300 μs, Duty Cycle ≤ 2%.

⁽²⁾ Switching characteristics are independent of operating junction temperature.

TYPICAL ELECTRICAL CHARACTERISTICS

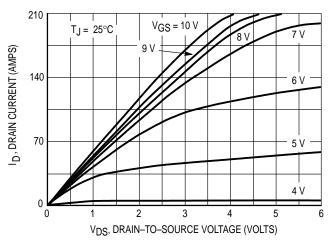


Figure 1. On-Region Characteristics

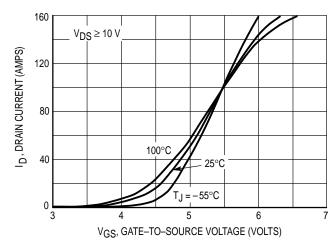


Figure 2. Transfer Characteristics

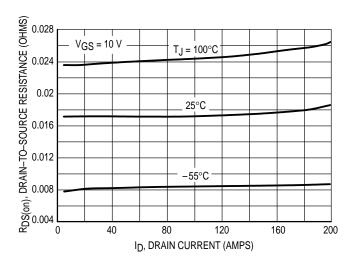


Figure 3. On–Resistance versus Drain Current and Temperature

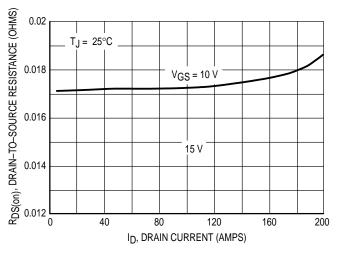


Figure 4. On–Resistance versus Drain Current and Gate Voltage

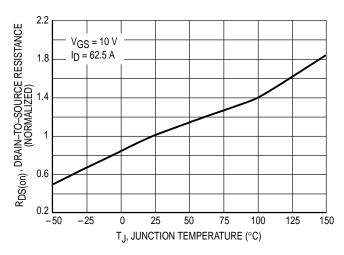


Figure 5. On–Resistance Variation with Temperature

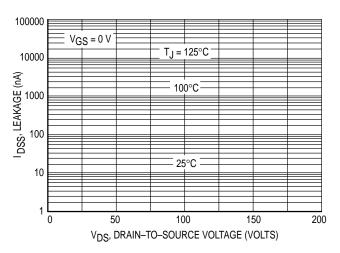


Figure 6. Drain-To-Source Leakage Current versus Voltage

POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain—gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_{G(AV)}$) can be made from a rudimentary analysis of the drive circuit so that

 $t = Q/I_{G(AV)}$

During the rise and fall time interval when switching a resistive load, VGS remains virtually constant at a level known as the plateau voltage, VSGP. Therefore, rise and fall times may be approximated by the following:

 $t_r = Q_2 \times R_G/(V_{GG} - V_{GSP})$

 $t_f = Q_2 \times R_G/V_{GSP}$

where

 V_{GG} = the gate drive voltage, which varies from zero to V_{GG} R_{G} = the gate drive resistance

and Q2 and VGSP are read from the gate charge curve.

During the turn—on and turn—off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

 $t_{d(on)} = R_G C_{iss} In [V_{GG}/(V_{GG} - V_{GSP})]$

 $t_{d(off)} = R_G C_{iss} In (V_{GG}/V_{GSP})$

The capacitance (C_{iss}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.

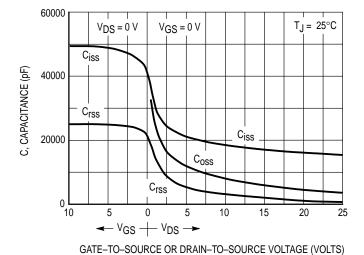
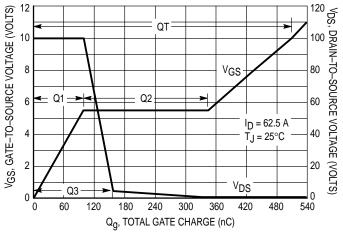


Figure 7. Capacitance Variation





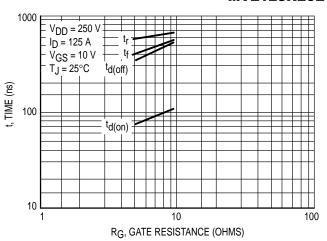


Figure 9. Resistive Switching Time Variation versus Gate Resistance

SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain—to—source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T_C) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance—General Data and Its Use."

Switching between the off–state and the on–state may traverse any load line provided neither rated peak current (I_{DM}) nor rated voltage (V_{DSS}) is exceeded and the transition time (t_r , t_f) do not exceed 10 μs . In addition the total power aver-

aged over a complete switching cycle must not exceed $(T_J(MAX) - T_C)/(R_{\theta}J_C)$.

A Power MOSFET designated E–FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non–linearly with an increase of peak current in avalanche and peak junction temperature.

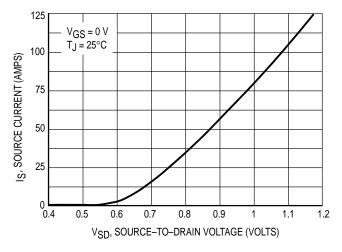
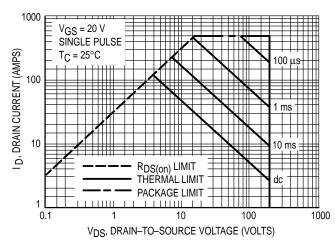


Figure 10. Diode Forward Voltage versus Current

SAFE OPERATING AREA



400 EAS, SINGLE PULSE DRAIN-TO-SOURCE AVALANCHE ENERGY (mJ) I_D = 125 A 350 300 250 200 150 100 50 25 75 100 125 150 TJ, STARTING JUNCTION TEMPERATURE (°C)

Figure 11. Maximum Rated Forward Biased Safe Operating Area

Figure 12. Maximum Avalanche Energy versus Starting Junction Temperature

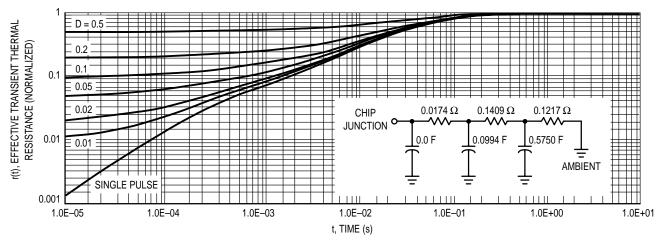


Figure 13. Thermal Response

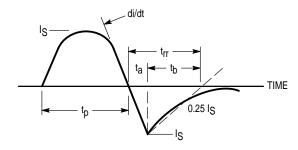
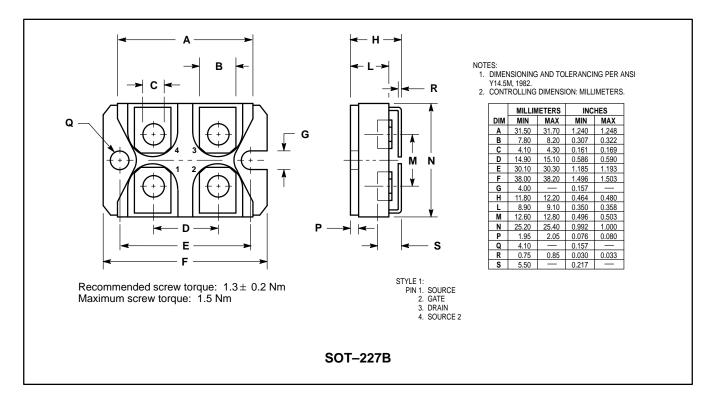


Figure 14. Diode Reverse Recovery Waveform

PACKAGE DIMENSIONS



Motorola reserves the right to make changes without further notice to any products herein. Motorola makes no warranty, representation or guarantee regarding the suitability of its products for any particular purpose, nor does Motorola assume any liability arising out of the application or use of any product or circuit, and specifically disclaims any and all liability, including without limitation consequential or incidental damages. "Typical" parameters can and do vary in different applications. All operating parameters, including "Typicals" must be validated for each customer application by customer's technical experts. Motorola does not convey any license under its patent rights nor the rights of others. Motorola products are not designed, intended, or authorized for use as components in systems intended for surgical implant into the body, or other applications intended to support or sustain life, or for any other application in which the failure of the Motorola product could create a situation where personal injury or death may occur. Should Buyer purchase or use Motorola products for any such unintended or unauthorized application, Buyer shall indemnify and hold Motorola and its officers, employees, subsidiaries, affiliates, and distributors harmless against all claims, costs, damages, and expenses, and reasonable attorney fees arising out of, directly or indirectly, any claim of personal injury or death associated with such unintended or unauthorized use, even if such claim alleges that Motorola was negligent regarding the design or manufacture of the part. Motorola and "A ere registered trademarks of Motorola, Inc. Motorola, Inc. is an Equal Opportunity/Affirmative Action Employer.

How to reach us: USA/EUROPE: Motorola Literature Distribution; P.O. Box 20912; Phoenix, Arizona 85036. 1–800–441–2447

Distribution; JAPAN: Nippon Motorola Ltd.; Tatsumi–SPD–JLDC, Toshikatsu Otsuki, 6. 1–800–441–2447 6F Seibu–Butsuryu–Center, 3–14–2 Tatsumi Koto–Ku, Tokyo 135, Japan. 03–3521–8315

MFAX: RMFAX0@email.sps.mot.com – TOUCHTONE (602) 244–6609 INTERNET: http://Design-NET.com

HONG KONG: Motorola Semiconductors H.K. Ltd.; 8B Tai Ping Industrial Park, 51 Ting Kok Road, Tai Po, N.T., Hong Kong. 852–26629298

